

# **ICC-ES Evaluation Report**

**ESR-1137** 

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**DIVISION: 03 00 00—CONCRETE** Section: 03 16 00—Concrete Anchors

**DIVISION: 05 00 00—METALS** 

Section: 05 05 19—Post-Installed Concrete Anchors

REPORT HOLDER:

**ITW RED HEAD** 

#### **EVALUATION SUBJECT:**

ITW RED HEAD EPCON G5 ADHESIVE ANCHORING SYSTEM FOR CRACKED AND UNCRACKED **CONCRETE** 

# 1.0 EVALUATION SCOPE

#### Compliance with the following codes:

- 2015, 2012, 2009, 2006 and 2003 International Building Code® (IBC)
- 2015, 2012, 2009, 2006 and 2003 International Residential Code® (IRC)
- 2013 Abu Dhabi International Building Code (ADIBC)†

†The ADIBC is based on the 2009 IBC. 2009 IBC code sections referenced in this report are the same sections in the ADIBC.

#### Property evaluated:

Structural

# **2.0 USES**

The Red Head Epcon G5 Adhesive Anchoring System is a post-installed adhesive anchorage system used to resist static, wind or earthquake (Seismic Design Categories A through F) tension and shear loads when installed in cracked and uncracked normal-weight concrete having a specified compressive strength, f'c, of 2500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

The anchoring system complies with anchors as described in Section 1901.3 of the 2015 IBC, Section 1909 of the 2012 IBC and is an alternative to cast-inplace anchors described in Section 1908 of the 2012 IBC, and Sections 1911 and 1912 of the 2009 and 2006 IBC and Sections 1912 and 1913 of the 2003 IBC. The anchoring system may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the IRC.

#### 3.0 DESCRIPTION

#### 3.1 General:

The Red Head Epcon G5 Adhesive Anchoring System

is a two-component, extended working time, structural epoxy adhesive, used with stud-type threaded rods and reinforcing bars installed in normal-weight concrete. The primary components of the Red Head Epcon G5 Adhesive Anchoring System are shown in Figure 1a of this report.

The manufacturer's printed installation instructions (MPII) are included with the adhesive package and are shown in Figure 2 of this report. The adhesive system must be used with the threaded rods and reinforcing bars described in Sections 3.2.4.1 and 3.2.4.2 of this report.

#### 3.2 Materials:

- 3.2.1 Adhesive: The Red Head Epcon G5 adhesive consists of two components, an epoxy resin and an amine-based hardener, packaged in 22-fluid-ounce (0.6 L) dual component cartridges. The adhesive components are mixed to a 1:1 ratio, by volume, using the nozzle supplied by Red Head. The original, unopened cartridges have an 18-month shelf life, as indicated by the "best used by" date stamped on the cartridge, when stored in a cool, dry, ventilated area at temperatures between 40°F and 90°F (5°C and 32°C) in accordance with the MPII.
- 3.2.2 Hole Cleaning Equipment: Hole cleaning equipment consists of wire brushes and air nozzles, as described in Figure 1a and Figure 2 of this report.
- 3.2.3 Dispensing Tools: Red Head Epcon G5 adhesive must be dispensed with manual or pneumatic dispensing tools provided by Red Head as described in Figure 1a.

### 3.2.4 Anchor Elements:

3.2.4.1 Threaded Steel Rods: The threaded steel rods must be clean, continuously threaded rods (allthread) ranging from 3/8 inch through 11/4 inches (9.5 mm through 31.75 mm) in diameter. Carbon steel threaded rods must comply with minimum ASTM A36 [minimum  $F_u = 58,000 \text{ psi } (400 \text{ MPa})$ ] or ASTM A193, Grade B7 [minimum  $F_u = 125,000$  psi (860 MPa)]. Stainless steel threaded rods must comply with ASTM F593 (Alloy Type 300, CW1 and CW2) [minimum  $F_u$  = 95,000 psi (655 MPa) for CW1, and  $F_u = 80,000$  psi (552 MPa) for CW2]. Table 1 notes steel design information for the threaded rods. Carbon steel threaded rods must be furnished with a 0.0002-inch-thick (5 µm) zinc electroplated coating complying with ASTM B633 SC1 or must be hot-dipped galvanized complying with ASTM A153, Class C or D.

Threaded steel rods must be straight and free from indentations or other defects along their length.



**3.2.4.2 Steel Reinforcing Bars:** Steel reinforcing bars are deformed reinforcing bars (rebar) as described in Table 2 of this report. The embedded portions of reinforcing bars must be straight, and free of mill scale, rust, mud, oil, and other coatings that impair the bond with the adhesive. Reinforcing bars must not be bent after installation except as set forth in ACI 318-14 Section 26.6.3.1(b) or ACI 318-11 Section 7.3.2, as applicable, with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.

**3.2.4.3 Ductility:** In accordance with ACI 318-14 2.3 or ACI 318-11 D.1, as applicable, in order for a steel element to be considered ductile, the tested elongation must be at least 14 percent and reduction of area must be at least 30 percent. Steel elements with a tested elongation of less than 14 percent or a reduction of area of less than 30 percent, or both, are considered brittle. Where values are nonconforming or unstated, the steel must be considered brittle.

#### 3.3 Concrete:

Normal-weight concrete must comply with Sections 1903 and 1905 of the IBC. The specified compressive strength of the concrete must be from 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa) [minimum of 24 MPa is required under ADIBC Appendix L, Section 5.1.1].

#### 4.0 DESIGN AND INSTALLATION

#### 4.1 Strength Design:

**4.1.1 General:** The design strength of anchors under the 2015 IBC, as well as 2015 IRC must be determined in accordance with ACI 318-14 and this report.

The design strength of anchors under the 2012, 2009, 2006 and 2003 IBC, as well as the 2012, 2009, 2006 and 2003 IRC, must be determined in accordance with ACI 318 (-11, -08, -05, -02) and this report.

A design example according to the 2012 IBC based on ACI 318-11 is given in Figure 1b of this report.

Design parameters are provided in Tables 1, 2, 3, 4, and 5 and references to ACI 318-14 for used with the 2015 IBC, and ACI 318-11 for use with the 2012IBC unless noted otherwise in Section 4.1.1 through 4.1.11 of this report.

The strength design of anchors must comply with ACI 318-14 17.3.1 or ACI 318-11 D.4.1, as applicable, except as required in ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable.

Strength reduction factors,  $\phi$ , as described in ACI 318-14 17.3.3 ACI 318-11 D.4.3, as applicable, must be used for load combinations calculated in accordance with Section 1605.2 of the IBC or ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, and given in tables 1 and 2 for the anchor element types included in this report. Strength reduction factors,  $\phi$ , as described in ACI 318-11 Section D.4.4, must be used for load combinations calculated in accordance with ACI 318-11 Appendix C.

- **4.1.2 Static Steel Strength in Tension:** The nominal static steel strength of a single anchor in tension,  $N_{sa}$ , in accordance with ACI 318-14 17.4.1.2 or ACI 318-11 D.5.1.2, as applicable, and the associated strength reduction factors,  $\phi$ , are provided in Tables 1 and 2 for the anchor element types included in this report.
- **4.1.3 Static Concrete Breakout Strength in Tension:** The nominal static concrete breakout strength of a single anchor or group of anchors in tension,  $N_{cb}$  or  $N_{cbg}$ , must be calculated in accordance with ACI 381-14

17.4.2 or ACI 318-11 D.5.2, as applicable with the following addition:

The basic concrete breakout strength of a single anchor in tension,  $N_b$ , must be calculated in accordance with ACI 318-14 17.4.2.2 or ACI 318-11 D.5.2.2, as applicable, using the values of  $k_{c,cr}$ , and  $k_{c,uncr}$  as described in Table 3 of this report. Where analysis indicates no cracking in accordance with ACI 318-14 17.4.2.6 or ACI 318-11 D.5.2.6, as applicable,  $N_b$  must be calculated using  $k_{c,uncr}$  and  $\Psi_{c,N}$  = 1.0. For anchors in lightweight concrete see ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable. The value of  $f_c$  used for calculation must be limited to 8,000 psi (55 MPa) in accordance with ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable. Additional information for the determination of nominal bond strength in tension is given in Section 4.1.4 of this report.

**4.1.4 Static Bond Strength in Tension:** The nominal static bond strength of a single adhesive anchor or group of adhesive anchors in tension,  $N_a$  or  $N_{ag}$ , must be calculated in accordance with ACI 318-14 17.4.5 or ACI 318-11 D.5.5, as applicable. Bond strength values are a function whether the concrete is cracked or uncracked, the concrete temperature range, the installation conditions (dry, water-saturated, water-filled holes, or submerged concrete), and the level of inspection provided. The resulting characteristic bond strength shall be multiplied by the associated strength reduction factor  $\phi_{nn}$  as follows:

CONCRETE TYPE	PERMISSIBLE INSTALLATION CONDITIONS	BOND STRENGTH	ASSOCIATED STRENGTH REDUCTION FACTOR	
	Dry	Tuncr	$\phi_{ m d}$	
Uncracked	Water-saturated	$ au_{uncr}$	φws	
Uncracked	Water-filled holes	Tuncr	$\phi_{ m wf}$	
	Submerged	Tuncr	$\phi_{sub}$	
	Dry	$ au_{cr}$	$\phi_{ m d}$	
Cracked	Water-saturated	Tcr	φws	
Cracked	Water-filled holes	Tcr	$\phi_{ m wf}$	
	Submerged	Tcr	$\phi_{sub}$	

Strength reduction factors for determination of the bond strength are given in Tables 4 and 5 of this report.

**4.1.5 Static Steel Strength in Shear:** The nominal static steel strength of a single anchor in shear as governed by the steel,  $V_{sa}$ , in accordance with ACI 318-14 17.5.1.2 or ACI 318-11 D.6.1.2, as applicable, and strength reduction factor,  $\phi$ , are given in Tables 1 and 2 for the anchor element types included in this report.

# **4.1.6 Static Concrete Breakout Strength in Shear:** The nominal static concrete breakout strength of a single anchor or group of anchors in shear, $V_{cb}$ or $V_{cbg}$ , must be calculated in accordance with ACI 318-14 17.5.2 or ACI 318-11 D.6.2, as applicable, based on information given in Table 3 of this report. The basic concrete breakout strength of a single anchor in shear, $V_b$ , must be calculated in accordance with ACI 318-14 17.5.2.2 or ACI 318-11 D.6.2.2, as applicable, using the values of d given in this report in lieu of $d_a$ (2015, 2012 and 2009 IBC) and $d_o$ (2006 IBC). In addition, $h_{ef}$ shall be substituted for $\ell_e$ . In no case shall $\ell_e$ exceed 8d. The

value of  $f_c$  must be limited to a maximum value of 8,000 psi (55 MPa) in accordance with ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable.

- **4.1.7 Static Concrete Pryout Strength in Shear:** The nominal static pryout strength of a single anchor or group of anchors in shear,  $V_{cp}$  or  $V_{cpg}$ , must be calculated in accordance with ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable.
- **4.1.8** Interaction of Tensile and Shear Forces: For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318-14 17.6 or ACI 318-11 D.7, as applicable.
- **4.1.9 Minimum Member Thickness,**  $h_{min}$ , **Minimum Anchor Spacing,**  $s_{min}$ , and **Minimum Edge Distance,**  $c_{min}$ : In lieu of ACI 318-14 17.7.1 and 17.7.3 or ACI 318-11 D.8.1 and D.8.3, respectively, as applicable, values of  $s_{min}$  and  $c_{min}$ , as given in Table 3 of this report, must be observed for anchor design and installation. The minimum member thicknesses  $h_{min}$  as given in Table 3 of this report must be observed for anchor design and installation. For adhesive anchors that will remain untorqued, ACI 318-14 17.7.4 or ACI 318-11 D.8.4, as applicable, applies.
- **4.1.10 Critical Edge Distance**  $c_{ac}$  and  $\psi_{cp,Na}$ : The modification factor  $\psi_{cp,Na}$ , must be determined in accordance with ACI 318-14 17.4.5.5 or ACI 318-11 D.5.5.5, as applicable, except as noted below:

For all cases where  $c_{Na}/c_{ac}$ <1.0,  $\psi_{cp,Na}$  determined from ACI 318-14 Eq. 17.4.5.5b or ACI 318-11 Eq. D-27, as applicable, need not be taken less than  $c_{Na}/c_{ac}$ . For all other cases,  $\psi_{cp,Na}$  shall be taken as 1.0.

The critical edge distance,  $c_{ac}$  must be calculated according to Eq. 17.4.5.5c for ACI 318-14 or Eq. D-27a for ACI 318-11, in lieu of ACI 318-14 17.7.6 or ACI 318-11 D.8.6, as applicable.

$$c_{ac} = h_{ef} \cdot \left(\frac{\tau_{k, uncr}}{1160}\right)^{0.4} \cdot \left[3.1 - 0.7 \frac{h}{h_{ef}}\right]$$

(Eq. 17.4.5.5c for ACI 318-14 or Eq. D-27a for ACI 318-11)

where

$$\left[\frac{h}{h_{cl}}\right]$$
 need not be taken as larger than 2.4; and

 $\tau_{k,uncr}$  = the characteristic bond strength stated in the tables of this report whereby  $\tau_{k,uncr}$  need not be taken as larger than:

$$au_{k,uncr} = rac{k_{uncr}\sqrt{h_{ef}f_c'}}{\pi \cdot d_a}$$
 Eq. (4-1)

**4.1.11 Design** Strength in Seismic Design Categories C, D, E and F: In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, anchors must be designed in accordance with ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable, except as described below. Modifications to the ACI 318-14 17.2.3 shall be applied under Section 1905.1.8 of the 2015 IBC. For the 2012 IBC, Section 1905.1.9 shall be omitted.

The nominal steel shear strength,  $V_{sa}$ , must be adjusted by  $\alpha_{V,seis}$  as given in Tables 1 and 2 for the anchor element types included in this report. The nominal bond strength  $\pi_{K,CT}$  must be adjusted by  $\alpha_{N,seis}$ , as given in Tables 4 and 5.

As an exception to ACI 318-11 D.3.3.4.2: Anchors designed to resist wall out-of-plane forces with design strengths equal to or greater than the force determined in accordance with ASCE 7 Equation 12.11-1 or 12.14-10 shall be deemed to satisfy ACI 318-11 D.3.3.4.3(d).

Under ACI 318-11 D.3.3.4.3(d), in lieu of requiring the anchor design tensile strength to satisfy the tensile strength requirements of ACI 318-11 D.4.1.1, the anchor design tensile strength shall be calculated from ACI 318-11 D.3.3.4.4.

The following exceptions apply to ACI 318-11 D.3.3.5.2:

- 1. For the calculation of the in-plane shear strength of anchor bolts attaching wood sill plates of bearing or non-bearing walls of light-frame wood structures to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3 need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:
  - 1.1. The allowable in-plane shear strength of the anchor is determined in accordance with AF&PA NDS Table 11E for lateral design values parallel to grain.
  - 1.2. The maximum anchor nominal diameter is  $^{5}/_{8}$  inch (16 mm).
  - 1.3. Anchor bolts are embedded into concrete a minimum of 7 inches (178 mm).
  - 1.4. Anchor bolts are located a minimum of  $1^{3}/_{4}$  inches (45 mm) from the edge of the concrete parallel to the length of the wood sill plate.
  - 1.5. Anchor bolts are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the wood sill plate.
  - 1.6. The sill plate is 2-inch or 3-inch nominal thickness.
- 2. For the calculation of the in-plane shear strength of anchor bolts attaching cold-formed steel track of bearing or non-bearing walls of light-frame construction to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3 need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:
  - 2.1. The maximum anchor nominal diameter is  $^{5}/_{8}$  inch (16 mm).
  - 2.2. Anchors are embedded into concrete a minimum of 7 inches (178 mm).
  - 2.3. Anchors are located a minimum of  $1^{3}/_{4}$  inches (45 mm) from the edge of the concrete parallel to the length of the track.
  - 2.4. Anchors are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the track.
  - 2.5. The track is 33 to 68 mil designation thickness.

Allowable in-plane shear strength of exempt anchors, parallel to the edge of concrete shall be permitted to be determined in accordance with AISI S100 Section E3.3.1.

3. In light-frame construction, bearing or nonbearing walls, shear strength of concrete anchors less than or equal to 1 inch [25 mm] in diameter attaching a sill plate or track to foundation or foundation stem wall need not satisfy ACI 318-11 D.3.3.5.3 (a) through (c) when the design strength of the anchors is determined in accordance with ACI 318-11 D.6.2.1(c).

#### 4.2 Allowable Stress Design:

**4.2.1 General:** For anchors designed using load combinations in accordance with IBC Section 1605.3 (Allowable Stress Design), allowable loads shall be established using Eq. (4-2) or Eq. (4-3):

$$T_{allowable,ASD} = \frac{\phi N_n}{\alpha}$$
 Eq. (4-2)

and

$$V_{allowable,ASD} = \frac{\phi V_n}{q}$$
 Eq. (4-3)

where:

Tallowable, ASD = Allowable tension load (lbf or kN)

Vallowable.ASD = Allowable shear load (lbf or kN)

- φN<sub>n</sub> = Lowest design strength of an anchor or anchor group in tension as determined in accordance with ACI 318-14 Chapter 17 and 2015 IBC Section 1905.1.8, ACI 318-11 Appendix D, ACI 318-08 Appendix D and 2009 IBC Sections 1908.1.9 and 1908.1.10, ACI 318-05 Appendix D and 2006 IBC Section 1908.1.16, and Section 4.1 of this report, as applicable (lbf or N).
- φV<sub>n</sub> = Lowest design strength of an anchor or anchor group in shear as determined in accordance with ACI 318-14 Chapter 17 and 2015 IBC Section 1905.1.8, ACI 318-11 Appendix D, ACI 318-08 Appendix D, and 2009 IBC Sections 1908.1.9 and 1908.1.10, ACI 318-05 Appendix D and 2006 IBC Section 1908.1.16, and Section 4.1 of this report, as applicable (lbf or N).
- $\alpha$  = Conversion factor calculated as a weighted average of the load factors for the controlling load combination. In addition,  $\alpha$  must include all applicable factors to account for non-ductile failure modes and required over-strength.

Limits on edge distance, anchor spacing and member thickness described in this report must apply.

Example calculations for derivation of  $T_{allowable,ASD}$  are provided in Table 6.

**4.2.2** Interaction of tensile and shear forces: In lieu of ACI 318-14 17.6.1, 17.6.2, 17.6.3 or ACI 318-11 D.7.1, D.7.2 and D.7.3, as applicable, interaction must be calculated as follows:

For shear loads  $V \le 0.2V_{allowable,ASD}$ , the full allowable load in tension,  $T_{allowable,ASD}$ , shall be permitted.

For tension loads  $T \le 0.2T_{allowable,ASD}$ , the full allowable load in shear,  $V_{allowable,ASD}$ , shall be permitted.

For all other cases:

$$\frac{T}{T_{allowable,ASD}} + \frac{V}{V_{allowable,ASD}} \le 1.2$$
 Eq. (4-4)

#### 4.3 Installation:

Installation parameters are illustrated in Figure 2 of this report. Installation must be in accordance with ACI 318-14 17.8.1 and 17.8.2; ACI 318-11 D.9.1 and D.9.2, as applicable. The anchors must be installed in accordance with the Red Head printed installation instructions, the plans and specifications approved by the code official, and the requirements of this report. The nozzles, brushes, and dispensing tools supplied by Red Head must be used along with the adhesive cartridges. See Figure 2 for brush specifications.

The adhesive anchoring system may be used for floor (vertically down) and wall (horizontal) applications. Overhead installations are beyond the scope of this report. Horizontal applications installed at a concrete or adhesive temperature above 70°F (21°C) require the use of a Red Head hole plug with the threaded rod or reinforcing bar.

#### 4.4 Special Inspection:

**4.4.1 General**: Installations may be made under continuous special inspection or periodic special inspection, as determined by the registered design professional. Tables 4 and 5 of this report provides strength reduction factors,  $\phi$ , corresponding to the type of inspection provided.

Continuous special inspection of adhesive anchors installed in horizontal orientations to resist sustained tension loads shall be performed in accordance with ACI 318-14 17.8.2.4 or ACI 318-11 D.9.2.4, as applicable. Installation in overhead or upwardly inclined oreintations is beyond the scope of this report.

Under the IBC, additional requirements as set forth in Sections 1705, 1706, or 1707 must be observed, where applicable.

4.4.2 Continuous Special Inspection for Proof Loading: Installations made under continuous special inspection with an on-site proof loading program must be performed in accordance with Section 1705.1.1 and Table 1705.3 of the 2015 and 2012 IBC, Section 1704.15 and Table 1704.4 of the 2009 IBC, or Section 1704.13 and Table 1704.4 of the 2006 and 2003 IBC, whereby periodic special inspection is defined in Section 1702.1 of the IBC and this report. The special inspector must be on the jobsite continuously during anchor installation to verify anchor type, adhesive expiration date, anchor dimensions, concrete type, concrete compressive strength, hole dimensions, hole cleaning procedures, anchor spacing, edge distances, concrete thickness, anchor embedment, tightening torque, and adherence to the manufacturer's printed installation instructions.

The proof loading program must be established by the registered design professional. As a minimum, the following requirements must be addressed in the proof loading program:

- Frequency of proof loading based on anchor type, diameter, and embedment.
- Proof loads by anchor type, diameter, embedment, and location.
- 3. Acceptable displacements at proof load.
- Remedial action in the event of a failure to achieve proof load, or excessive displacement.

Unless otherwise directed by the registered design professional, proof loads must be applied as confined tension tests. Proof load levels must not exceed the lesser of 67 percent of the load corresponding to the nominal bond strength as calculated from the characteristic bond stress for uncracked concrete modified for edge effects and concrete properties, or 80 percent of the minimum specified anchor element yield strength  $(A_{\text{Se},N} \ f_{\text{ya}})$ . The proof load shall be maintained at the required load level for a minimum of 10 seconds.

**4.4.3 Periodic Special Inspection**: Periodic special inspection must be performed where required in accordance with Section 1705.1.1 and Table 1705.3 of

the 2015 and 2012 IBC, Section 1704.15 and Table 1704.4 of the 2009 IBC, Section 1704.13 and Table 1704.4 of the 2006, and 2003 IBC, whereby periodic special inspection is defined in Section 1702.1 of the IBC, and this report. The special inspector must be on the jobsite initially during anchor installation to verify anchor type, adhesive expiration date, anchor dimensions, concrete type, concrete compressive strength, hole dimensions, hole cleaning procedures, anchor spacing, edge distances, concrete thickness, anchor embedment, tightening torque, and adherence to the manufacturer's printed installation instructions. The special inspector must verify the initial installations of type and size of adhesive anchor by construction personnel on the site. Subsequent installations of the same anchor type and size by the same construction personnel are permitted to be performed in the absence of the special inspector. Any change in the anchor product being installed or the personnel performing the installation requires an initial inspection. For ongoing installations over an extended period, the special inspector must make regular inspections to confirm correct handling and installation of the product.

#### 5.0 CONDITIONS OF USE

The Red Head Epcon G5 Adhesive Anchoring System described in this report is a complies with or is a suitable alternative to what is specified in the codes listed in Section 1.0 of this report, subject to the following conditions:

- 5.1 The Red Head Epcon G5 Adhesive must be installed in accordance with the manufacturer's printed installation instructions, as included with the adhesive packaging and described in Figure 2 of this report.
- **5.2** The anchors must be installed in cracked or uncracked normal-weight concrete having a specified compressive strength of  $f_c$ '= 2500 psi to 8500 psi (17.2 MPa to 58.6 Mpa) [minimum of 24 MPA is required under ADIBC Appendix L, Section 5.1.1].
- **5.3** The values of  $f_c$  used for calculation purposes must not exceed 8,000 psi (55 Mpa).
- 5.4 Anchors must be installed in concrete base materials in holes predrilled in accordance with the instructions provided in Figure 2 of this report, using a carbide-tipped masonry drill bit manufactured within the range of the maximum and minimum drilltip dimensions of ANSI B212.15-1994.
- 5.5 Loads applied to the anchors must be adjusted in accordance with Section 1605.2 of the IBC for strength design and in accordance with Section 1605.3 of the IBC for allowable stress design.
- 5.6 Red Head Epcon G5 adhesive anchors are recognized for use in resisting short- and long-term loads, including wind and earthquake loads, subject to the conditions of this report.
- 5.7 In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, anchor strength must be adjusted in accordance with Section 4.1.11 of this report.
- 5.8 Red Head Epcon G5 adhesive anchors are permitted to be installed in concrete that is cracked or that may be expected to crack during the service life of the anchor, subject to the conditions of this report.

- **5.9** Strength design values must be established in accordance with Section 4.1 of this report.
- **5.10** Allowable stress design values must be established in accordance with Section 4.2 of this report.
- 5.11 Minimum anchor spacing and edge distance, as well as minimum member thickness, must comply with the values given in this report.
- 5.12 Prior to anchor installation, calculations and details demonstrating compliance with this report shall be submitted to the code official. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- 5.13 Anchors are not permitted to support fire-resistive construction. Where not otherwise prohibited by the code, anchors are permitted for installation in fireresistive construction, provided at least one of the following conditions is fulfilled:
  - Anchors are used to resist wind or seismic forces only.
  - Anchors that support gravity load-bearing structural elements are within a fire-resistive envelope or a fire-resistive membrane, are protected by approved fire-resistive materials, or have been evaluated for resistance to fire exposure in accordance with recognized standards.
  - Anchors are used to support nonstructural elements.
- 5.14 Since an ICC-ES acceptance criteria for evaluating data to determine the performance of adhesive anchors subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report.
- 5.15 Use of zinc-plated carbon steel threaded rods or steel reinforcing bars is limited to dry, interior locations.
- 5.16 Use of hot-dipped galvanized carbon steel and stainless steel rods is permitted for exterior exposure or damp environments.
- 5.17 Steel anchoring materials in contact with preservative-treated and fire-retardant-treated wood must be of zinc-coated carbon steel or stainless steel. The minimum coating weights for zinc-coated steel must comply with ASTM A153.
- 5.18 Special inspection must be provided in accordance with Section 4.4 of this report. Continuous special inspection for anchors installed in horizontal orientations to resist sustained tension loads must be provided in accordance with Section 4.4.4.2 of this report.
- **5.19** Installation of anchors in orientations to resist sustained tension loads shall be performed by personnel certified by an applicable certification program in accordance with ACI 318-14 17.8.2.2 or 17.8.2.3, or ACI 318-11 D.9.2.2 or D.9.2.3, as applicable.
- **5.20** Epcon G5 Adhesive Anchors is limited to resist tension and shear forces in floor installations only provided the installation is within base material temperature of 70 degrees F and 110 degrees F. Overhead (vertically upward) and upwardly inclined installations are beyond the scope of this report.

5.21 Epcon G5 Adhesive is manufactured by Red Head in Elk Grove Village, Illinois, under a quality control program with inspections by ICC-ES.

#### **6.0 EVIDENCE SUBMITTED**

Data in accordance with the ICC-ES Acceptance Criteria for Post-installed Adhesive Anchors in Concrete Elements (AC308), dated January 2016, which incorporates requirements in ACI 355.4-11; and quality control documentation.

#### 7.0 IDENTIFICATION

7.1 The Red Head Epcon G5 adhesive is identified by labels on the adhesive cartridges bearing the adhesive manufacturer's name (ITW Commercial

- Construction North America) and address (Glendale Heights, Illinois), the product name (Red Head Epcon G5), best-used-by expiration date, and the evaluation report number (ESR-1137).
- **7.2** The report holder's contact information is the following:

ITW RED HEAD 700 HIGH GROVE BOULEVARD GLENDALE HEIGHTS, ILLINOIS 60139 (800) 848-5611

www.itw-redhead.com techsupport@itwccna.com

TABLE 1—STEEL DESIGN INFORMATION FOR FRACTIONAL THREADED ROD

		avuna.			N	OMINAL R	OD DIAME	TER, d (inc	h)	
Ó	CHARACTERISTIC	SYMBOL	UNITS	<sup>3</sup> / <sub>8</sub>	1/2	<sup>5</sup> / <sub>8</sub>	3/4	<sup>7</sup> / <sub>8</sub>	1	11/4
Threaded area	rod effective cross-sectional	A <sub>se</sub>	inch²	0.078	0.142	0.226	0.335	0.462	0.606	0.969
	Nominal steel strength in tension	N <sub>sa</sub>	lb	4,500	8,230	13,110	19,400	26,780	35,130	56,210
136	Nominal steel strength in shear	V <sub>sa</sub>	lb	2,250	4,940	7,870	11,640	16,070	21,080	33,730
Carbon Steel A36	Strength reduction factor for tension, steel failure mode <sup>1</sup>	φ	-	0.75	0.75	0.75	0.75	0.75	0.75	0.75
Carbo	Strength reduction factor for shear, steel failure mode <sup>1</sup>	φ	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	Reduction factor for seismic shear	α <sub>V,seis</sub>	-	0.70	0.70	0.70	0.70	0.70	0.70	0.70
	Nominal steel strength in tension	N <sub>sa</sub>	lb	9,690	17,740	28,250	41,810	57,710	75,710	121,140
93 B7	Nominal steel strength in shear	V <sub>sa</sub>	lb	4,845	10,640	16,950	25,090	34,630	45,430	72,680
Carbon Steel A193 B7	Strength reduction factor for tension, steel failure mode <sup>1</sup>	φ	-	0.75	0.75	0.75	0.75	0.75	0.75	0.75
Carbon	Strength reduction factor for shear, steel failure mode <sup>1</sup>	φ	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	Reduction factor for seismic shear	$\alpha_{V,seis}$	-	0.70	0.70	0.70	0.70	0.70	0.70	0.70
	F593 CW1 nominal steel strength in tension	N <sub>sa</sub>	lb	7,365	13,480	21,470	-	-	-	-
	F593 CW1 nominal steel strength in shear	V <sub>sa</sub>	lb	3,680	6,740	10,735	-	-	-	-
F593	F593 CW2 nominal steel strength in tension	N <sub>sa</sub>	lb	-	-	-	25,385	35,110	46,055	73,645
Steel	F593 CW2 nominal steel strength in shear	V <sub>sa</sub>	lb	-	-	-	12,690	17,555	23,030	36,820
Stainless Steel F593	Strength reduction factor for tension, steel failure mode <sup>1</sup>	φ	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65
S	Strength reduction factor for shear, steel failure mode <sup>1</sup>	φ	-	0.60	0.60	0.60	0.60	0.60	0.60	0.60
	Reduction factor for seismic shear	α <sub>V,seis</sub>	-	0.70	0.70	0.70	0.70	0.70	0.70	0.70

For **SI**: 1 inch = 25.4mm, 1 lbf = 4.45N

<sup>&</sup>lt;sup>1</sup> The tabulated value of  $\phi$  applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, are used as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4.

TABLE 2—STEEL DESIGN INFORMATION FOR FRACTIONAL REINFORCING BAR

(	CHARACTERISTIC		UNITS	NOMINAL REINFORCING BAR (REBAR) SIZE							
`	MANAGILMONG	SYMBOL	UNITS	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 10	
Nominal bar diameter		d	in.	3/8	1/2	5/8	3/4	7/8	1	1 <sup>1</sup> / <sub>4</sub>	
Reinforcing sectional a	g bar effective cross- irea	A <sub>se</sub>	in²	0.11	0.2	0.31	0.44	0.6	0.79	1.27	
	Nominal steel strength in tension	N <sub>sa</sub>	lb	9,900	18,000	27,900	39,600	54,000	71,100	114,300	
le 60	Nominal steel strength in shear	V <sub>sa</sub>	lb	5,940	10,800	16,740	23,760	32,400	42,660	68,580	
15 Grade	Strength reduction factor for tension, steel failure mode <sup>1</sup>	φ	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65	
ASTM 615	Strength reduction factor for shear, steel failure mode <sup>1</sup>	φ	-	0.60	0.60	0.60	0.60	0.60	0.60	0.60	
·	Reduction factor for seismic shear	$lpha_{V,seis}$	-	0.91	0.91	0.91	0.90	0.90	0.71	0.71	

For **SI:** 1 inch = 25.4mm, 1 lbf = 4.45N, 1ft-lbf = 1.356 N-M, 1 psi = 0.006895 MPa.

TABLE 3—CONCRETE BREAKOUT DESIGN INFORMATION FOR FRACTIONAL THREADED ROD AND REINFORCING BAR

			NOMIN	AL ROD D	IAMETER A	AND REINF	ORCING E	BAR SIZE,	d (inch)
CHARACTERISTIC	SYMBOL	UNITS	<sup>3</sup> / <sub>8</sub>	1/2	<sup>5</sup> / <sub>8</sub>	3/4	<sup>7</sup> / <sub>8</sub>	1	11/4
			No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 10
Effectiveness factor for uncracked concrete	<b>K</b> <sub>c,uncr</sub>	-	24	24	24	24	24	24	24
Effectiveness factor for cracked concrete	<b>K</b> <sub>c,cr</sub>	-	17	17	17	17	17	17	17
Minimum concrete thickness <sup>2</sup>	h <sub>min</sub>	in.	$h_{ef} + 1^{1}/_{4}$ $h_{ef} + 2d_{o}$						
Anchor embedment depth - minimum	h <sub>ef,min</sub>	in.	2 <sup>3</sup> / <sub>8</sub>	23/4	31/8	31/2	31/2	4	5
Anchor embedment depth - maximum	h <sub>ef,max</sub>	in.	33/8	41/2	5 <sup>5</sup> / <sub>8</sub>	63/4	7 <sup>7</sup> / <sub>8</sub>	9	11 <sup>1</sup> / <sub>4</sub>
Minimum spacing	S <sub>min</sub>	in.	<sup>15</sup> / <sub>16</sub>	1	21/2	6	31/2	4	5
Minimum edge distance	C <sub>min</sub>	in.	<sup>15</sup> / <sub>16</sub>	1	21/2	6	31/2	4	5
Critical edge distance	Cac	in.	See Section 4.1.10 of this report						
Strength reduction factor for tension, concrete failure mode <sup>1</sup>	φ	Cond. B	0.65	0.65	0.65	0.65	0.65	0.65	0.65
Strength reduction factor for shear, concrete failure mode <sup>1</sup>	φ	Cond. B	0.70	0.70	0.70	0.70	0.70	0.70	0.70

For **SI**: 1 inch = 25.4mm, 1 lbf = 4.45N

<sup>&</sup>lt;sup>1</sup>The tabulated value of  $\phi$  applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4.

<sup>&</sup>lt;sup>1</sup> The tabulated value of  $\phi$  applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, are used and the requirements of ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4 for Condition B.

TABLE 4—RED HEAD EPCON G5 ADHESIVE ANCHOR BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL THREADED ROD<sup>1</sup>

01	IADAOTEDIOTIO	SYMBOL	LINUTO			NOMINA	ROD DIAM	IETER (inch	)	
CH	CHARACTERISTIC SYI		UNITS	<sup>3</sup> / <sub>8</sub>	1/2	<sup>5</sup> / <sub>8</sub>	3/4	<sup>7</sup> / <sub>8</sub>	1	11/4
minimun		h <sub>ef,min</sub>	in.	2 <sup>3</sup> / <sub>8</sub>	23/4	31/8	31/2	31/2	4	5
Anchor e	embedment depth – m	h <sub>ef,max</sub>	in.	33/8	41/2	5 <sup>5</sup> / <sub>8</sub>	63/4	7 <sup>7</sup> / <sub>8</sub>	9	11 <sup>1</sup> / <sub>4</sub>
Temperature Range A <sup>2,3,4</sup>	Characteristic Bond Strength for Uncracked Concrete	$T_{k,uncr}$	psi	1,155	1,155	1,155	1,155	1,155	1,155	1,155
Tempe Range	Characteristic Bond Strength for Cracked Concrete <sup>5</sup>	$T_{k,cr}$	psi	475	560	560	560	560	560	560
tion	Strength Reduction Factor – Dry Concrete	$\phi$ dry, ci	-	0.65	0.65	0.65	0.65	0.55	0.55	0.55
Continuous Inspection	Strength Reduction Factor – Water Saturated Concrete	$\phi_{ extsf{ws, ci}}$	ı	0.65	0.65	0.65	0.65	0.55	0.55	0.55
tinuous	Strength Reduction Factor – Water- Filled Holes	Фwf, ci	ı	0.65	0.65	0.65	0.65	0.55	0.55	0.55
Con	Strength Reduction Factor – Submerged Concrete	$\phi_{sub,ci}$	ı	0.65	0.65	0.65	0.65	0.65	0.55	0.55
uo	Strength Reduction Factor – Dry Concrete	$\phi_{ ext{dry, pi}}$		0.55	0.55	0.55	0.55	0.45	0.45	0.45
nspection	Strength Reduction Factor – Water Saturated Concrete	Øws, pi	-	0.55	0.55	0.55	0.55	0.45	0.45	0.45
Periodic Inspection	Strength Reduction Factor – Water- Filled Holes	$\phi_{wf,\;pi}$	-	0.55	0.55	0.55	0.55	0.45	0.45	0.45
Ъ	Strength Reduction Factor – Submerged Concrete	$\phi$ sub, pi	1	0.55	0.55	0.55	0.55	0.55	0.45	0.45
Reduction tension	on factor for seismic	α <sub>N,seis</sub>	-				0.80			

For **SI:** 1 inch = 25.4mm, 1 lbf = 4.45N, 1ft-lbf = 1.356 N-M, 1 psi = 0.006895 MPa.

<sup>&</sup>lt;sup>1</sup> Bond strength values correspond to concrete compressive strength range 2,500 psi to 8,500 psi [minimum of 24 MPa is required under ADIBC Appendix L, Section 5.1.1].

<sup>&</sup>lt;sup>2</sup> Temperature range A: Maximum short term temperature of 130 degrees F and maximum long term temperature of 110 degrees F.

<sup>&</sup>lt;sup>3</sup> Short term elevated concrete temperatures are those that occur over brief interval, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>&</sup>lt;sup>4</sup> For load combinations consisting of only short-term loads, such as wind or seismic loads, bond strengths may be increased 36% for Temperature Range A.

<sup>&</sup>lt;sup>5</sup> For structures assigned to IBC or IRC Seismic Design Category C, D, E, or F, bond strength values must be multiplied by α<sub>N,seis</sub>.

# TABLE 5—RED HEAD EPCON G5 ADHESIVE ANCHOR BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL REINFORCING BAR<sup>1</sup>

					NOI	MINAL REIN	IFORCING I	BAR (REBAF	R) SIZE	
СН	IARACTERISTIC	SYMBOL	UNITS	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 10
minimun		h <sub>ef,min</sub>	in.	2 <sup>3</sup> / <sub>8</sub>	23/4	31/8	31/2	31/2	4	5
Anchor e maximur	embedment depth – m	h <sub>ef,max</sub>	in.	33/8	41/2	5 <sup>5</sup> / <sub>8</sub>	63/4	7 <sup>7</sup> / <sub>8</sub>	9	11 <sup>1</sup> / <sub>4</sub>
Temperature Range A <sup>2,3,4</sup>	Characteristic Bond Strength for Uncracked Concrete	$T_{k,uncr}$	psi	1,155	1,155	1,155	1,155	1,155	1,155	1,155
Tempe Range	Characteristic Bond Strength for Cracked Concrete <sup>5</sup>	$T_{k,cr}$	psi	475	560	560	560	560	560	560
tion	Strength Reduction Factor – Dry Concrete	Фdry, ci	-	0.65	0.65	0.65	0.65	0.55	0.55	0.55
Continuous Inspection	Strength Reduction Factor – Water Saturated Concrete	$\phi$ ws, ci	1	0.65	0.65	0.65	0.65	0.55	0.55	0.55
tinuous	Strength Reduction Factor – Water- Filled Holes	Øwf, ci	1	0.65	0.65	0.65	0.65	0.55	0.55	0.55
Con	Strength Reduction Factor – Submerged Concrete	$\phi_{sub,ci}$	-	0.65	0.65	0.65	0.65	0.65	0.55	0.55
uo	Strength Reduction Factor – Dry Concrete	$\phi_{dry,\;pi}$	,	0.55	0.55	0.55	0.55	0.45	0.45	0.45
nspecti	Strength Reduction Factor – Water Saturated Concrete	Øws, pi	-	0.55	0.55	0.55	0.55	0.45	0.45	0.45
Periodic Inspection	Strength Reduction Factor – Water- Filled Holes	$\phi_{wf,\;pi}$	-	0.55	0.55	0.55	0.55	0.45	0.45	0.45
Pe	Strength Reduction Factor – Submerged Concrete	Фsub, pi	-	0.55	0.55	0.55	0.55	0.55	0.45	0.45
Reduction tension	on factor for seismic	$a_{N,seis}$	-				0.80	-	-	-

For **SI:** 1 inch = 25.4mm, 1 lbf = 4.45N, 1ft-lbf = 1.356 N-M, 1 psi = 0.006895 MPa.

<sup>2</sup> Temperature range A: Maximum short term temperature of 130 degrees F and maximum long term temperature of 110 degrees F.

<sup>&</sup>lt;sup>5</sup> For structures assigned to IBC or IRC Seismic Design Category C, D, E, or F, bond strength values must be multiplied by  $\alpha_{N.seis}$ .



<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength range 2,500 psi to 8,500 psi [minimum of 24MPa is required under ADIBC Appendix L, Section 5.1.1].

<sup>&</sup>lt;sup>3</sup> Short term elevated concrete temperatures are those that occur over brief interval, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>&</sup>lt;sup>4</sup> For load combinations consisting of only short-term loads, such as wind or seismic loads, bond strengths may be increased 36% for Temperature Range A.

# TABLE 6—EXAMPLE RED HEAD EPCON G5 ADHESIVE ALLOWABLE STRESS DESIGN VALUES (ASD) FOR ILLUSTRATIVE PURPOSES

Anchor Diameter (d)	Min/Max Embedment Depth, h <sub>ef</sub> (in)	Char. Bond Strength $\tau_{k,uncr}$ (psi)	Allowable Tension Load (lb) 2500psi	Controlling Failure Mode
31	2 <sup>3</sup> / <sub>8</sub>	1,155	1,420	Bond
<sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>	1,155	2,016	Bond
1,	2 <sup>3</sup> / <sub>4</sub>	1,155	2,190	Bond
1/2	41/2	1,155	3,584	Bond
5.1	31/8	1,155	2,911	Concrete
<sup>5</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	1,155	5,600	Bond
31	31/2	1,155	3,451	Concrete
3/4	6 <sup>3</sup> / <sub>4</sub>	1,155	8,064	Bond
71	31/2	1,155	3,451	Concrete
<sup>7</sup> / <sub>8</sub>	7 <sup>7</sup> / <sub>8</sub>	1,155	10,975	Bond
	4	1,155	4,216	Concrete
1	9	1,155	14,230	Concrete
41/	5	1,155	5,892	Concrete
11/4	11 <sup>1</sup> / <sub>4</sub>	1,155	19,887	Concrete

For **SI:** 1 inch = 25.4mm, 1 lbf = 4.45N, 1ft-lbf = 1.356 N-M, 1 psi = 0.006895 MPa.

This table was developed based on the following conditions:

<sup>&</sup>lt;sup>1</sup>Single anchor with static tension only, A36 threaded rod

<sup>&</sup>lt;sup>2</sup>Vertical downward installation direction

<sup>&</sup>lt;sup>3</sup>Inspection regimen = Periodic

<sup>&</sup>lt;sup>4</sup>Installation temperature = 70°F to 110°F

<sup>&</sup>lt;sup>5</sup>Long term temperature = 110°F

<sup>&</sup>lt;sup>6</sup>Short term temperature = 130°F

<sup>&</sup>lt;sup>7</sup>Dry hole condition (carbide drilled hole)

<sup>&</sup>lt;sup>8</sup>Embedment = hef (min/max for each diameter)

<sup>&</sup>lt;sup>9</sup>Concrete determined to remain uncracked for the life of the anchorage

<sup>&</sup>lt;sup>10</sup>Load combinations from ACI 318-11 Section 9.2 (no seismic loading)

<sup>1130%</sup> dead load and 70% live load, controlling load combination 1.2D + 1.6L

<sup>&</sup>lt;sup>12</sup>Calculation of weighted average for  $\alpha = 0.3*1.2 + 0.7*1.6 = 1.48$ 

 $<sup>^{13}</sup>f_c = 2,500 \text{ psi (normal weight concrete)}$ 

 $<sup>^{14}</sup>C_{a1} = C_{a2} \ge C_{ac}$ 

 $<sup>^{15}</sup>h \ge h_{min}$ 

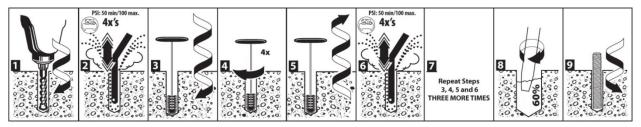
# Illustrative Procedure to Verify Applied Tension Load does not exceed Allowable Stress Design Tension Value:

Red Head Epcon G5 Adhesive Anchor  $^{1}/_{2}$ -inch diameter, with an embedment of  $4^{1}/_{2}$  inches, assuming the conditions given in Table 6 (for use with the 2012 IBC, based on ACI 318-11 Appendix D). Applied Tension load,  $N_{ua}$  = 4,000 lbs.

	PROCEDURE	CALCULATION
Step 1	Calculate steel strength of a single anchor in tension per ACI 318-11 D.5.1.2 and Table 1 of this report.	$\phi N_{sa} = 0.75*8,230 = 6,173$ lbs steel strength
Step 2	Calculate concrete breakout strength of a single anchor in tension per ACI 318-11 D.5.2 and Table 3 of this report.	$N_b = k_{c,uncr}^* \lambda_a \sqrt{f_c} h_{ef}^{1.5} = 24*1.0* \sqrt{2,500}^* 4.5^{1.5}$ $N_b = 11,455 \text{ lbs}$ $\phi N_{cb} = \phi A_{NC}/A_{NCO} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b$ $\phi N_{cb} = 0.65*1.0*1.0*1.0*11,455$ $\phi N_{cb} = 7,446 \text{ lbs concrete breakout strength}$
Step 3	Calculate bond strength of a single anchor in tension per ACI 318-11 D.5.5 and Table 4 of this report.	$N_{ba} = \lambda_a  \tau_{k,uncr}  \pi d h_{ef}$ $N_{ba} = 1.0^* 1,155^* 3.14^* 0.5^* 4.5$ $N_{ba} = 8,160  \text{lbs}$ $\phi N_a = \phi  A_{Na} / A_{Na0}  \psi_{ed,Na}  \psi_{cp,Na}  N_{ba}$ $\phi N_a = 0.65^* 1.0^* 1.0^* 8,160$ $\phi N_a = 5,305  \text{lbs}  \text{bond strength}$
Step 4	Determine compliance with required anchor strength per ACI 318-11 D.4.1.	$\phi N_{sa} = 6,173 \text{ lbs} > N_{ua} = 4,000 \text{ lbs}$ $\phi N_{cb} = 7,446 \text{ lbs} > N_{ua} = 4,000 \text{ lbs}$ $\phi N_{ao} = 5,305 \text{ lbs} > N_{ua} = 4,000 \text{ lbs}$
Step 5	Calculate allowable stress design conversion factor for loading condition per ACI 318-11 Section 9.2.	$\alpha = 1.2D + 1.6L = 1.2(0.3) + 1.6(0.7) = 1.48$
Step 6	Calculate allowable stress design value per Section 4.2 of this report.	$T_{allowable,ASD} = \phi N_n / \alpha = 5,305 \text{ lbs/1.48}$ $T_{allowable,ASD} = 3,585 \text{ lbs allowable stress design}$

FIGURE 1b—EXAMPLE DESIGN CALCULATION

#### **EPCON G5 ADHESIVE ANCHOR INSTALLATION INSTRUCTIONS**



#### STEP 1

- Use a rotary hammer drill or pneumatic air drilling machine with a drill bit complying to ANSI B212.15.1994 tolerance standards.
- Use a drill bit equal to the threaded rod/rebar diameter plus <sup>1</sup>/<sub>16</sub>" (for <sup>3</sup>/<sub>8</sub>" & <sup>1</sup>/<sub>2</sub>" diameter anchors) and <sup>1</sup>/<sub>8</sub>" (for <sup>5</sup>/<sub>8</sub>" diameter & larger anchors). Drill hole to the required embedment depth. See attached table for the minimum/maximum embedment depths.
- The G5 Adhesive Anchors are for use with wall and floor installations only. Wall installations may be used with <sup>3</sup>/<sub>8</sub>" thru maximum <sup>3</sup>/<sub>4</sub>" diameter threaded rod/rebar.
- Per construction specification, adhere to minimum spacing, minimum edge distance, and minimum member thickness.

#### STEP 2

- Oscillate a clean air nozzle in and out of the dry, damp, water-filled or submerged hole four times, for a total of four seconds, starting at the bottom of the hole with contaminant-free compressed air, exhausting hole until visually clean (i.e. no drill dust, debris, etc.).
- If required, use an extension on the end of the air nozzle to reach the bottom of the hole.

#### STEP 3

- Select an appropriately sized Red Head brush from part nos. SB038, SB012, SB058, SB034, SB078, SB010, SB125, or match brush color coding to anchor diameter. Brush must be checked for wear before use. See attached table for brush specifications, including minimum diameter.
- Insert brush into the hole with a clockwise motion. For every <sup>1</sup>/<sub>2</sub>" forward advancement, complete one full turn until bottom of hole is reached. For faster and more suitable cleaning, attach the brush to a drill.
- If required, use a wire brush extension (part nos. ESDS-38 or EHAN-38) to reach the bottom of the hole.

#### STEP 4

• Twist/spin the brush four full turns at bottom of hole.

#### STEP 5

- Using a clockwise motion, for every full turn of the brush, pull the brush <sup>1</sup>/<sub>2</sub>" out of the hole.
- Air-clean the dust off the brush to prevent clogging of brush.

#### STEP 6

- Oscillate a clean air nozzle in and out of the dry, damp, water-filled or submerged hole four times, for a total of four seconds, starting at the bottom of the hole with contaminant-free compressed air, exhausting hole until visually clean (i.e. no drill dust, debris, etc.).
- If required, use an extension on the end of the air nozzle to reach the bottom of the hole.

#### STEP 7

 Repeat steps 3, 4, 5, and 6 (brushing and blowing) three more times before proceeding to Step 8.

#### STEP 8

- Check the "best used by" date on cartridge and that the cartridge has been stored in temperatures between 40°F and 90°F. Review Material Safety Data Sheet (MSDS) before use.
- Assemble Red Head supplied cartridge (part no. G5-22) and nozzle (part no. E55).
- Place assembly into a hand injection tool (part no. E102) or pneumatic tool (part no. E202).
- Dispense mixed adhesive outside of hole until uniform color is achieved.
- During floor installations, concrete and adhesive must be between 70°F to 110°F or artificially maintained.
- During wall installations, concrete and adhesive must be between 70°F to 110°F or artificially maintained.
- For wall (horizontal) installations with concrete or adhesive over 70°F, the anchor rod/rebar must be marked with the required embedment depth and assembled with a Red Head hole plug positioned on the rod/rebar at the required embedment depth.
- Insert the nozzle to the bottom of the hole and inject the
  adhesive at an angle leaving the nozzle tip always slightly
  below the fill level. In a slow circular direction, work the
  adhesive into the sides of the hole, filling slowly to ensure
  proper adhesive distribution, until the hole is approximately
  60% filled.

#### STEP 9

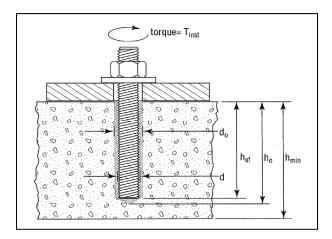
- Immediately insert and oil, rust and scale free threaded rod/rebar to the required embedment depth. Use a counterclockwise motion to ensure proper adhesive distribution.
- After installing the anchor, the gap between the threaded rod/rebar and the concrete must be completely filled with adhesive. The adhesive must fill voids, crevices and uniformly coat the threaded rod/rebar and concrete.
- For holes that contain water, keep injecting the adhesive below the water in order to displace the water upward.
- After installation, do not disturb the anchor until the full cure time has elapsed.
- Adhesive must be fully cured before applying any load or torque.

#### SPECIFICATIONS FOR INSTALLATION OF RED HEAD EPCON G5 ADHESIVE ANCHORS IN CONCRETE

			NOMINAL ROD DIAMETER (inch) AND REINFORCING BAR SIZE						
CHARACTERISTIC	SYMBOL	UNITS	3/8	1/2	<sup>5</sup> / <sub>8</sub>	3/4	7/8	1	11/4
			No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 10
Nominal carbide bit diameter	d <sub>o</sub>	in.	<sup>7</sup> / <sub>16</sub>	<sup>9</sup> / <sub>16</sub>	3/4	7/8	1	1 <sup>1</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>8</sub>
Anchor embedment depth - minimum	h <sub>ef, min</sub>	in.	2 <sup>3</sup> / <sub>8</sub>	23/4	31/8	31/2	31/2	4	5
Anchor embedment depth - maximum	h <sub>ef, max</sub>	in.	33/8	41/2	5 <sup>5</sup> / <sub>8</sub>	63/4	77/8	9	11 <sup>1</sup> / <sub>4</sub>
Minimum spacing	S <sub>min</sub>	in.	<sup>15</sup> / <sub>16</sub>	1	21/2	6	31/2	4	5
Minimum edge distance	C <sub>min</sub>	in.	<sup>15</sup> / <sub>16</sub>	1	21/2	6	31/2	4	5
Minimum concrete thickness	h <sub>min</sub>	in.	$h_{ef} + 1^{1}/_{4}$ $h_{ef} + 2d_{o}$						
Maximum tightening torque for pretension clamping	T <sub>inst</sub>	ft lb	9	16	47	90	145	170	370

For **SI:** 1 inch = 25.4mm, 1 lbf = 4.45N, 1ft-lbf = 1.356N-m, 1psi = 0.006895MPa.

#### **ANCHOR INSTALLATION**



#### **BRUSH SPECIFICATIONS**

Brush color	Part No.	Anchor diameter (in) (d)	Rebar size (d)	Drill bit diameter (in) (d <sub>o</sub> )	Minimum brush diameter (in) (d <sub>brush</sub> )
Grey	SB038	3/8	No. 3	<sup>7</sup> / <sub>16</sub>	0.563
Brown	SB012	1/2	No. 4	<sup>9</sup> / <sub>16</sub>	0.675
Green	SB058	<sup>5</sup> / <sub>8</sub>	No. 5	3/4	0.900
Yellow	SB034	3/4	No. 6	7/8	1.125
Red	SB078	7/8	No. 7	1	1.350
Purple	SB010	1	No. 8	1 <sup>1</sup> / <sub>8</sub>	1.463
Blue	SB125	11/4	No. 10	1 <sup>3</sup> / <sub>8</sub>	1.575

# GEL TIMES AND CURE TIMES FOR RED HEAD EPCON G5 ADHESIVE

Concrete Temp. (°F) <sup>1,2</sup>	Gel Time (minutes) <sup>3</sup>	Cure Time (hours) <sup>4</sup>
70	15	24
90	9	24
110	9	24

For **SI:**  $t^{\circ}$  (°F-32) X .555 = °C.

- <sup>1</sup> Adhesive must be installed in base material temperatures of 70°F to 110°F or artificially maintained.
- <sup>2</sup> Cartridge temperature should not differ significantly from the temperature of the base material.
- <sup>3</sup> Gel time is the maximum time from the end of mixing to when the insertion of the anchor into the adhesive shall be completed.
- <sup>4</sup> Cure time is the minimum time from the end of gel time to when the anchor maybe torqued or loaded. Anchors are to be undisturbed during the cure time.



# **ICC-ES Evaluation Report**

# **ESR-1137 FBC Supplement**

Reissued March 2020

This report is subject to renewal March 2021.

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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

DIVISION: 05 00 00-METALS

Section: 05 05 19—Post-Installed Concrete Anchors

**REPORT HOLDER:** 

**ITW RED HEAD** 

**EVALUATION SUBJECT:** 

#### ITW RED HEAD EPCON G5 ADHESIVE ANCHORING SYSTEM FOR CRACKED AND UNCRACKED CONCRETE

#### 1.0 REPORT PURPOSE AND SCOPE

#### Purpose:

The purpose of this evaluation report supplement is to indicate that Red Head Epcon G5 Adhesive Anchoring System for Cracked and Uncracked Concrete, recognized in ICC-ES evaluation report ESR-1137, has also been evaluated for compliance with the codes noted below.

#### Compliance with the following codes:

- 2014 and 2010 Florida Building Code—Building
- 2014 and 2010 Florida Building Code—Residential

#### 2.0 PURPOSE OF THIS SUPPLEMENT

This supplement is issued to indicate that the Red Head Epcon G5 Adhesive Anchoring System for Cracked and Uncracked Concrete described in Sections 2.0 through 7.0 of the evaluation report, ESR-1137, complies with the 2014 and 2010 Florida Building Code—Building and the 2014 and 2010 Florida Building Code—Residential, when designed and installed in accordance with the 2012 International Building Code® (IBC) provisions noted in the evaluation report under the following conditions:

- Design wind loads must be based on Section 1609 of the 2014 or 2010 Florida Building Code—Building or Section 301.2.1.1 of the 2014 or 2010 Florida Building Code—Residential, as applicable.
- Load combinations must be in accordance with Section 1605.2 or Section 1605.3 of the 2014 or 2010 Florida Building Code—Building, as applicable.
- The modifications to ACI 318-11 as shown in the 2009 IBC Sections 1908.1.9 and 1908.1.10, as noted in 2009 IBC Section 1912.1, do not apply to the 2010 Florida Building Code.

Use of the Red Head Epcon G5 Adhesive Anchoring System for Cracked and Uncracked Concrete described in the evaluation report, for compliance with the High-Velocity Hurricane Zone provisions of the 2014 or 2010 Florida Building Code—Building and the 2014 or 2010 Florida Building Code—Residential has not been evaluated, and is outside the scope of this supplement.

For products falling under Florida Rule 9N-3, verification that the report holder's quality assurance program is audited by a quality assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official when the report holder does not possess an approval by the Commission).

This supplement expires concurrently with the evaluation report, reissued March 2020.

